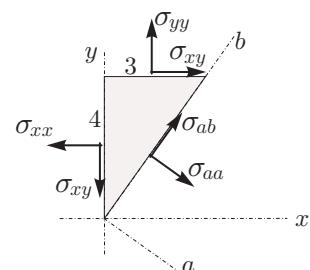
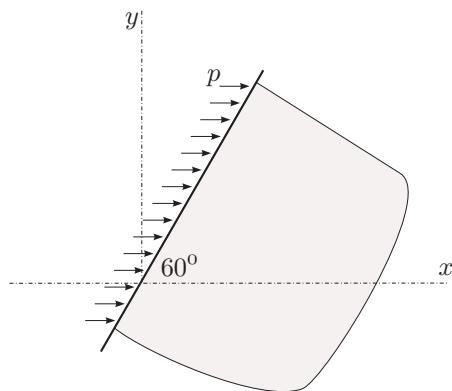


## TRDNOST (VSŠ) - 1. KOLOKVIJ (18. 11. 2014)

Pazljivo preberite besedilo vsake naloge! Pišite čitljivo! Uspešno reševanje!

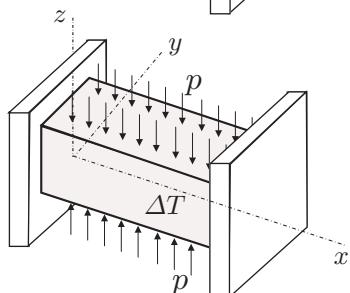
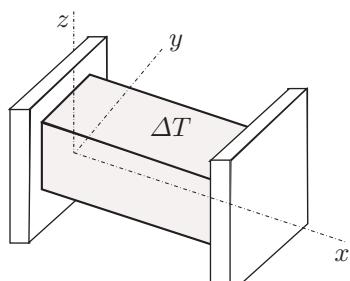
naloga	točk
1	
2	
3	
4	

1. Deformiranje nekega telesa lahko opišemo s pomiki oblike  $\vec{u} = 10^{-3} (xy, z + 2x, y^2 - x)$ . Določite:i) tenzor majhnih deformacij v točki  $T(1, -1, 0)$ ;ii) specifično spremembo dolžine vlakna v točki  $T(1, -1, 0)$  v smeri  $\vec{a} = 2\vec{e}_x + 1\vec{e}_y$ ! (20%)2. V tanki trikotni ploščici vlada homogeno ravninsko napetostno stanje. Znane so napetosti  $\sigma_{xx}$ ,  $\sigma_{aa}$  in  $\sigma_{ab}$ . Določite napetostni tenzor v koordinatah  $x, y, z$ ! (20%)Podatki:  $\sigma_{xx} = 20 \text{ MPa}$ ,  $\sigma_{aa} = 60 \text{ MPa}$ , $\sigma_{ab} = -30 \text{ MPa}$ .3. Na rob tanke stene, ki leži pod kotom  $60^\circ$  glede na os  $x$ , deluje enakomerna površinska obtežba velikosti  $p = 20 \text{ kN/cm}^2$ , kot kaže slika. Napetosti so konstantne po celotni prostornini stene. Normalna deformacija v navpični smeri znaša  $\epsilon_{yy} = 1 \cdot 10^{-3}$ .Določite napetostni tenzor v koordinatah  $x, y, z$ ! (30%)Podatki:  $\nu = 0.25$ ,  $E = 2 \cdot 10^5 \text{ MPa}$ .4. Kvader iz izotropnega, linearno elastičnega materiala postavimo med dve togji plošči in se grejemo za  $\Delta T$ . Določite:

i) Napetostni tenzor zaradi spremembe temperature!

ii) Ob enaki spremembi temperature ploskvi z normalama  $\vec{e}_z$  in  $-\vec{e}_z$  obremenimo z enakomerno zvezno tlačno obtežbo  $p$ .

Kolikšna mora biti obtežba, da se volumen kvadra ne spremeni?

iii) Deformacijski tenzor za dano spremembo temperature in izračunano obtežbo  $p$ ! (30%)Podatki:  $\nu = 0.2$ ,  $E = 2 \cdot 10^4 \text{ kN/cm}^2$ ,  $\alpha = 10^{-5} \text{ K}^{-1}$ ,  $\Delta T = 30 \text{ K}$ .

## 1. Naloga

$$\text{i.) } \vec{\epsilon} = 10^{-3} \begin{bmatrix} y & x & 0 \\ 2 & 0 & 1 \\ -1 & 2y & 0 \end{bmatrix} \quad \hat{\vec{\epsilon}} = 10^{-3} \begin{bmatrix} y & 1+\frac{x}{2} & -\frac{1}{2} \\ \sin x & 0 & y+\frac{1}{2} \\ 0 & 0 & 0 \end{bmatrix}$$

$$\vec{\epsilon}_T = 10^{-3} \begin{bmatrix} -1 & \frac{3}{2} & -\frac{1}{2} \\ \frac{3}{2} & 0 & -\frac{1}{2} \\ -\frac{1}{2} & -\frac{1}{2} & 0 \end{bmatrix}$$

$$\text{ii.) Daa } \approx 10^{-3} \begin{bmatrix} \frac{2}{\sqrt{5}} & \frac{1}{\sqrt{5}} & 0 \end{bmatrix} \begin{bmatrix} -1 & \frac{3}{2} & -\frac{1}{2} \\ \frac{3}{2} & 0 & -\frac{1}{2} \\ -\frac{1}{2} & -\frac{1}{2} & 0 \end{bmatrix} \begin{bmatrix} \frac{2}{\sqrt{5}} \\ \frac{1}{\sqrt{5}} \\ 0 \end{bmatrix} = 10^{-3} \begin{bmatrix} \frac{2}{\sqrt{5}} & \frac{1}{\sqrt{5}} & 0 \end{bmatrix} \begin{bmatrix} -\frac{1}{2\sqrt{5}} \\ \frac{6}{2\sqrt{5}} \\ -\frac{3}{2\sqrt{5}} \end{bmatrix}$$

$$= 10^{-3} \left( -1 + \frac{6}{10} \right) = 4 \cdot 10^{-4}$$

## 2. Naloga

$$\vec{\epsilon}_A = \frac{4}{5} \vec{\epsilon}_x - \frac{3}{5} \vec{\epsilon}_y$$

$$\vec{\epsilon}_B = \frac{3}{5} \vec{\epsilon}_x + \frac{4}{5} \vec{\epsilon}_y$$

$$60 = \begin{bmatrix} \frac{4}{5} & -\frac{3}{5} \end{bmatrix} \begin{bmatrix} 20 & 6_{xy} \\ 6_{xy} & 6_{yy} \end{bmatrix} \begin{bmatrix} \frac{4}{5} \\ -\frac{3}{5} \end{bmatrix}$$

$$1500 = [4 \ -3] \begin{bmatrix} 80 - 36_{xy} \\ 46_{xy} - 36_{yy} \end{bmatrix} = 320 + 96_{yy} - 246_{xy}$$

$$96_{yy} - 246_{xy} = 1180$$

$$\begin{aligned} 6_{xy} &= -\frac{70}{3} \\ 6_{yy} &= \frac{620}{9} \\ 6_{xy} &= -23.3 \text{ MPa} \\ 6_{yy} &= 68.9 \text{ MPa} \end{aligned}$$

$$-30 = \begin{bmatrix} \frac{3}{5} & \frac{4}{5} \end{bmatrix} \begin{bmatrix} 20 & 6_{xy} \\ 6_{xy} & 6_{yy} \end{bmatrix} \begin{bmatrix} \frac{4}{5} \\ -\frac{3}{5} \end{bmatrix}$$

$$-750 = [3 \ 4] \begin{bmatrix} 80 - 36_{xy} \\ 46_{xy} - 36_{yy} \end{bmatrix} = 240 - 126_{yy} + 76_{xy}$$

$$-126_{yy} + 76_{xy} = -990$$

## 3. Naloga

$$\text{a.) Deformacije: } \epsilon_{yy} = 1 \cdot 10^{-3}$$

b.) Napetosti:

$$6_{xx} = 6_{yy} = 6_{zz} = 0 ; \begin{bmatrix} 6_{xx} & 6_{xy} \\ 6_{xy} & 6_{yy} \end{bmatrix} \begin{bmatrix} -\frac{\sqrt{3}}{2} \\ \frac{1}{2} \end{bmatrix} = \begin{bmatrix} 20 \\ 0 \end{bmatrix}$$

$$\begin{aligned} -\frac{\sqrt{3}}{2} 6_{xx} + \frac{1}{2} 6_{xy} &= 20 \cdot \frac{\sqrt{3}}{2} \\ -\frac{\sqrt{3}}{2} 6_{xy} + \frac{1}{2} 6_{yy} &= 0 \end{aligned}$$

c.) Hooke-ov zakon

$$E = 2 \cdot 10^5 \text{ MPa} = 2 \cdot 10^4 \text{ kN/cm}^2$$

$$\epsilon_{xx} = \frac{1+\nu}{E} 6_{xx} - \frac{\nu}{E} (6_{xx} + 6_{yy})$$

$$10^{-3} = \epsilon_{yy} = \frac{1+\nu}{E} 6_{yy} - \frac{\nu}{E} (6_{xx} + 6_{yy}) \Rightarrow -2 6_{xx} + 6_{yy} = 10^{-3} E$$

$$\epsilon_{zz} = -\frac{\nu}{E} (6_{xx} + 6_{yy})$$

$$-0.25 6_{xx} + 6_{yy} = 20$$

$$\begin{aligned} 6_{xx} &= -149 \text{ kN/cm}^2 \\ 6_{yy} &= 155 \text{ kN/cm}^2 \end{aligned}$$

$$6_{xy} = 8.9 \text{ kN/cm}^2$$

$$\text{G} = \begin{bmatrix} -149 & 8.9 \\ 8.9 & 155 \end{bmatrix} [\text{kN/cm}^2]$$

4. Naloga

i.) deformacije:  $\epsilon_{xx} = 0$

$$\text{napetosti: } [\sigma] \begin{bmatrix} 0 \\ 0 \end{bmatrix} = 0 \quad [\sigma] \begin{bmatrix} 0 \\ 0 \end{bmatrix} = 0$$

$$\sigma_{xy} = \sigma_{yy} = \sigma_{yz} = 0 \quad \sigma_{xz} = \sigma_{yz} = \sigma_{zz} = 0$$

Hookeov zakon

$$0 = \epsilon_{xx} = \frac{1+\nu}{E} \sigma_{xx} - \frac{\nu}{E} \sigma_{yy} + \alpha_T \Delta T \Rightarrow \sigma_{xx} = -E \alpha_T \Delta T = -2 \cdot 10^4 \cdot 10^{-5} \cdot 30$$

$$\sigma = \begin{bmatrix} -6 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \text{ kN/cm}^2$$

$$\sigma_{xx} = -6 \text{ kN/cm}^2$$

ii) deformacije  $\epsilon_{xx} = 0 ; \epsilon_y = 0 \Rightarrow \epsilon_{yy} + \epsilon_{zz} = 0$

$$\text{napetosti: } [\sigma] \begin{bmatrix} 0 \\ 0 \end{bmatrix} = 0 \quad [\sigma] \begin{bmatrix} 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ -\nu \end{bmatrix}$$

$$\sigma_{xy} = \sigma_{yy} = \sigma_{yz} = 0 \quad \sigma_{xz} = \sigma_{yz} = 0 \quad \sigma_{zz} = -\nu$$

Hookeov zakon

$$0 = \epsilon_{xx} = \frac{1+\nu}{E} \sigma_{xx} - \frac{\nu}{E} (\sigma_{yy} - \nu) + \alpha_T \Delta T$$

$$\epsilon_{yy} = \frac{1+\nu}{E} \cdot 0 - \frac{\nu}{E} (\sigma_{xx} - \nu) + \alpha_T \Delta T \quad \left. \right\} +$$

$$\epsilon_{zz} = \frac{1+\nu}{E} \cdot (-\nu) - \frac{\nu}{E} (\sigma_{xx} - \nu) + \alpha_T \Delta T \quad \left. \right\} +$$

$$0 = \epsilon_{yy} + \epsilon_{zz} = -\frac{1+\nu}{E} \nu - \frac{2\nu}{E} (\sigma_{xx} - \nu) + 2\alpha_T \Delta T$$

$$\sigma_{xx} + \nu \nu = -E \alpha_T \Delta T$$

$$-2\nu \sigma_{xx} + (\nu - 1)\nu = -2E \alpha_T \Delta T$$

$$\sigma_{xx} + 0.2\nu = -6 \cdot 0.4$$

$$-0.4 \sigma_{xx} - 0.8\nu = -12$$

$$-0.72\nu = -14.4 \Rightarrow \nu = 20 \text{ kN/cm}^2$$

iii.)  $\epsilon_{xx} = 0$

za  $\epsilon_{yy}$  in  $\epsilon_{zz}$  poštevamo  $\sigma_{xx}$ :

$$\sigma_{xx} = -10 \text{ kN/cm}^2$$

$$\epsilon_{yy} = -\frac{\nu}{E} (-30) + \alpha_T \Delta T = 6 \cdot 10^{-4}$$

$$\epsilon_{zz} = -\frac{1+\nu}{E} 20 - \frac{\nu}{E} (-30) + \alpha_T \Delta T = -6 \cdot 10^{-4}$$

KONTROLA  $\epsilon_{yy} + \epsilon_{zz} = 0$

$$\hat{\sigma} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 6 & 0 \\ 0 & 0 & -6 \end{bmatrix}$$