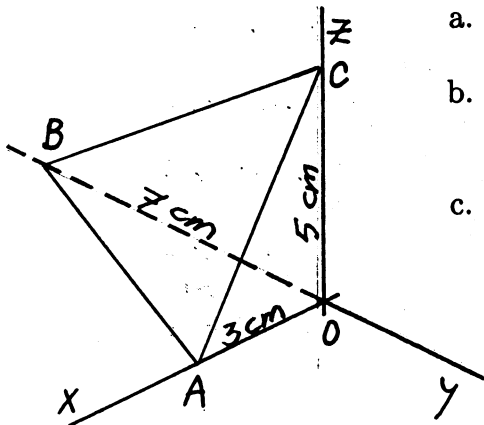


1. Na poševno mejno ploskev ABC prikazane elementarne piramide deluje enakomerna površinska obtežba $\vec{q} = 13.982 \vec{e}_x + 6.439 \vec{e}_y + 1.610 \vec{e}_z$ [kN/cm²]. Napetostna vektorja v koordinatnih ravninah $y = 0$ in $z = 0$ sta $\vec{\sigma}_y = \sigma_{yx} \vec{e}_x$ in $\vec{\sigma}_z = \sigma_{zx} \vec{e}_x - 10 \vec{e}_z$.



- Določi vse komponente tenzorja napetosti v koordinatnem sistemu x, y, z !
- Razstavi tenzor napetosti na hidrostatični in deviatorični del ter ob upoštevanju Misesovega kriterija plastičnega tečenja preveri, ali je elementarna piramida v elastičnem območju!
- Določi dolžino stranice \overline{AO} po deformaciji piramide!

$E = 21\,000 \text{ kN/cm}^2$

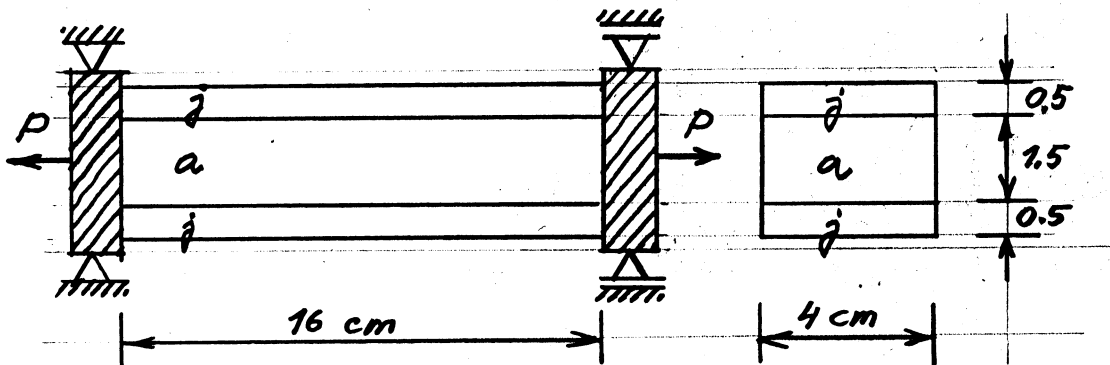
$\sigma_Y = 36 \text{ kN/cm}^2$

$\nu = 0.3$

(40 točk)

2. Dve jekleni in ena aluminijaska lamela so prosto sestavljene v prizmo in na obeh osnovnih ploskvah nepodajno priključene na absolutno togi plošči. Največja natezna normalna napetost, ki lahko nastopi v jekleni lameli, je $[\sigma_j] = 165 \text{ MPa}$, v aluminijski pa $[\sigma_a] = 60 \text{ MPa}$.

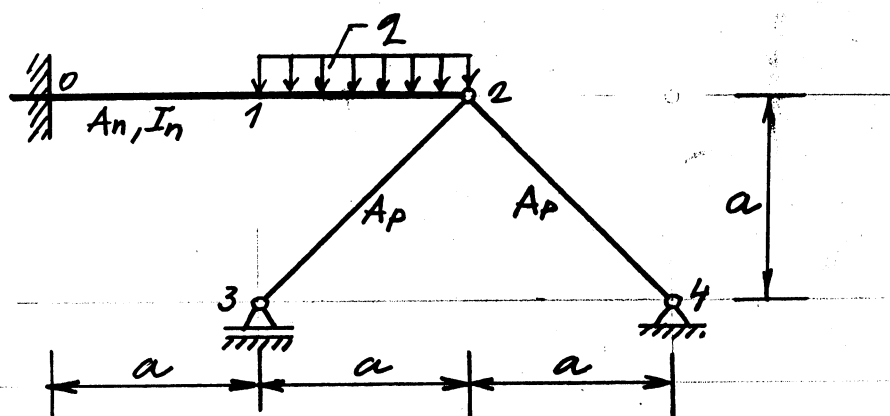
- Določi dopustno natezno silo $[P]$ tako, da v nobeni od lamel ne bo presežena dovoljena vzdolžna normalna napetost.
- Določi napetosti v lamelah, če je $P = 0$ in segrejemo prizmo za $\Delta T = 80 \text{ K}$.



$E_j = 2.1 \cdot 10^5 \text{ MPa}$
 $E_a = 0.7 \cdot 10^5 \text{ MPa}$
 $\alpha_j = 1.25 \cdot 10^{-5} / \text{K}$
 $\alpha_a = 2.00 \cdot 10^{-5} / \text{K}$

(30 točk)

2. Določi osni sili v palicah $\overline{23}$ in $\overline{24}$ v odvisnosti od obtežbe q !



$E = 200\,000 \text{ MPa}$
 $A_p = 0.0008 \text{ m}^2$
 $A_n = 0.0100 \text{ m}^2$
 $I_n = 0.0002 \text{ m}^4$
 $a = 4 \text{ m}$

(40 točk)

Ad 1.) Ebene ABC:

$$\frac{x}{3} - \frac{y}{7} + \frac{z}{5} = 1 \rightarrow \phi = 35x - 15y + 21z - 105 = 0$$

$$\vec{n} = 35\vec{e}_x - 15\vec{e}_y + 21\vec{e}_z$$

$$|\vec{n}| = \sqrt{35^2 + 15^2 + 21^2} = 43,486$$

$$\vec{e}_n = \frac{\vec{n}}{n} \rightarrow \vec{e}_n = 0,805\vec{e}_x - 0,345\vec{e}_y + 0,483\vec{e}_z$$

$$\sigma_{zz} = -10, \quad \sigma_{yy} = \sigma_{yz} = 0$$

$$a) \begin{Bmatrix} p_{mx} \\ p_{my} \\ p_{mz} \end{Bmatrix} = \begin{Bmatrix} 13,982 \\ 6,439 \\ 1,610 \end{Bmatrix} = \begin{bmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & 0 & 0 \\ \sigma_{zx} & 0 & -10 \end{bmatrix} \begin{Bmatrix} 0,805 \\ -0,345 \\ 0,483 \end{Bmatrix}$$

$$0,805 \sigma_{xx} - 0,345 \sigma_{xy} + 0,483 \sigma_{xz} = 13,982$$

$$0,805 \sigma_{xy} = 6,439 \rightarrow \sigma_{xy} = 8 \text{ kN/cm}^2$$

$$0,805 \sigma_{xz} - 0,483 \cdot 10 = 1,610 \rightarrow \sigma_{xz} = 8 \text{ kN/cm}^2$$

$$\rightarrow 0,805 \sigma_{xx} = 13,982 + 0,345 \cdot 8 - 0,483 \cdot 8$$

$$\sigma_{xx} = 16 \text{ kN/cm}^2$$

$$[\sigma_{ij}] = \begin{bmatrix} 16 & 8 & 8 \\ 8 & 0 & 0 \\ 8 & 0 & -10 \end{bmatrix}$$

$$I_1^{\sigma} = 16 - 10 = 6$$

$$\sigma^H = \frac{1}{3} I_1^{\sigma} \rightarrow \sigma^H = 2$$

$$b) [\sigma_{ij}^H] = \begin{bmatrix} 2 & 0 & 0 \\ 0 & 2 & 0 \\ 0 & 0 & 2 \end{bmatrix}$$

$$[\Delta_{ij}^H] = \begin{bmatrix} 14 & 8 & 8 \\ 8 & -2 & 0 \\ 8 & 0 & -12 \end{bmatrix}$$

$$I_2^s = \begin{vmatrix} -2 & 0 \\ 0 & -12 \end{vmatrix} + \begin{vmatrix} 14 & 8 \\ 8 & -12 \end{vmatrix} + \begin{vmatrix} 14 & 8 \\ 8 & -2 \end{vmatrix} \rightarrow \boxed{I_2^s = -300}$$

$$f(\lambda) = |I_2^s| - k_M^2 \quad \dots \quad k_M = \frac{5Y}{\sqrt{3}}$$

$$f(\lambda) = 300 - \frac{36^2}{3} = -132 \rightarrow \boxed{EZ. ST. !}$$

c) $\frac{1+\nu}{E} = 6,19 \cdot 10^{-5} ; \quad \frac{\nu}{E} = 1,43 \cdot 10^{-5}$

$$\epsilon_{ij} = \frac{1+\nu}{E} \sigma_{ij} - \frac{\nu}{E} I_1^s \delta_{ij}$$

$$\epsilon_{xx} = 10^{-5} (6,19 \cdot 16 - 1,43 \cdot 6) \rightarrow \epsilon_{xx} = 90,476 \cdot 10^{-5}$$

$$\overline{AO} : \quad \overline{AO}' = (1 + \epsilon_{xx}) \cdot \overline{AO} \rightarrow \boxed{\overline{AO}' = 3,0027 \text{ cm}}$$

Ad 2.)

$$\epsilon_j = \epsilon_a$$

$$A_j = 2 \text{ cm}^2$$

$$A_a = 6 \text{ cm}^2$$

$$a) \quad \epsilon_j = \frac{\sigma_j}{E_j}, \quad \epsilon_a = \frac{\sigma_a}{E_a}$$

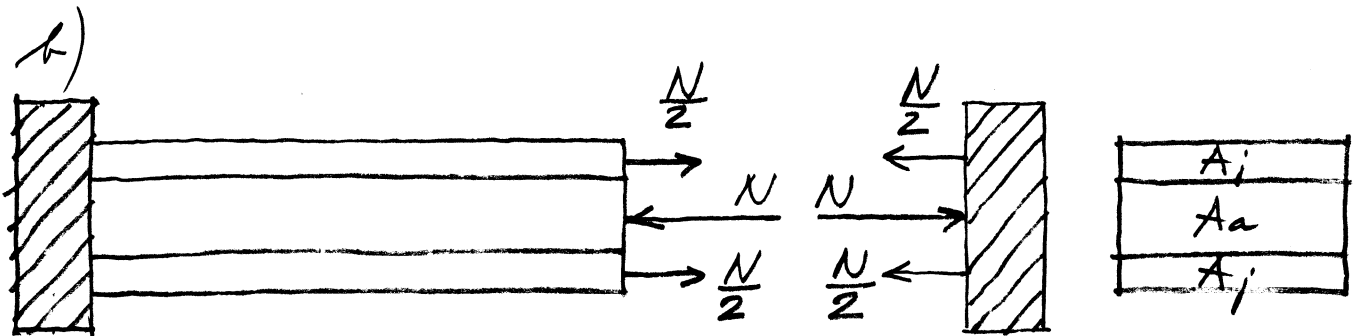
$$\epsilon_j = \epsilon_a \rightarrow \frac{\sigma_j}{E_j} = \frac{\sigma_a}{E_a} \rightarrow \sigma_a = \sigma_j \frac{E_a}{E_j}$$

$$P = 2 \sigma_j A_j + \sigma_a A_a = \sigma_j \left(2A_j + \frac{E_a}{E_j} A_a \right)$$

$$[P_j] = [\sigma_j] \left(2A_j + \frac{E_a}{E_j} A_a \right) = 0,099 \text{ MN}$$

$$[P_a] = [\sigma_a] \left(A_a + 2A_j \frac{E_j}{E_a} \right) = 0,108 \text{ MN}$$

$$[P] = [P_j] = 0,099 \text{ MN}$$



$$\epsilon_j = \frac{N}{2E_j A_j} + \alpha_j \Delta T \quad ; \quad \epsilon_a = \frac{-N}{E_a A_a} + \alpha_a \Delta T$$

$$\epsilon_j = \epsilon_a \rightarrow \frac{N}{2E_j A_j} + \alpha_j \Delta T = -\frac{N}{E_a A_a} + \alpha_a \Delta T$$

$$N \frac{2E_j A_j + E_a A_a}{2E_j E_a A_j A_a} = (\alpha_a - \alpha_j) \Delta T$$

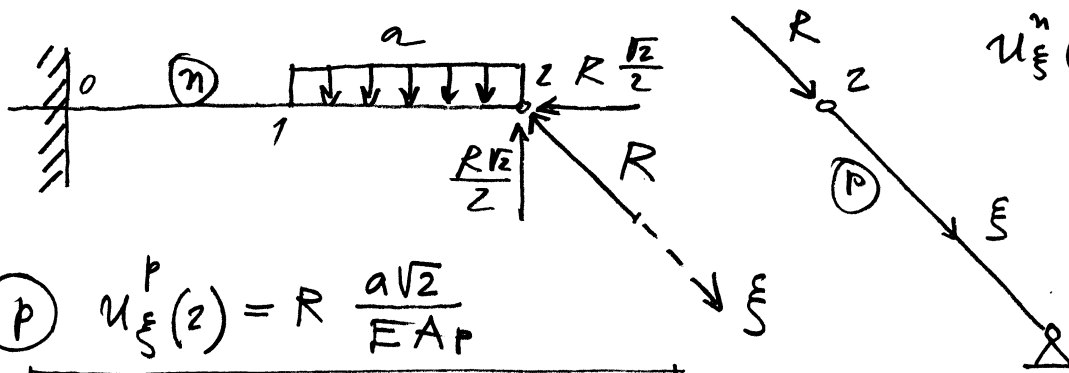
$$N = \frac{2E_j A_j E_a A_a}{2E_j A_j + E_a A_a} (\alpha_a - \alpha_j) \Delta T \rightarrow N = 0,0168 \text{ MN}$$

$$\sigma_a = \frac{-0,0168 \cdot 10^4}{6} \rightarrow \sigma_a = -28 \text{ MPa}$$

$$\sigma_j = \frac{0,0168 \cdot 10^4}{2 \cdot 2} \rightarrow \sigma_j = 42 \text{ MPa}$$

3.)

$N_{23} = 0!$



$u_{\xi}^n(2) = u_{\xi}^p(2)!$

(p) $u_{\xi}^p(2) = R \frac{a\sqrt{2}}{EA_p}$

$u_{\xi}^p(2) = 0,03536 R$

(n) $u_x^{(n)}(2) = -R \frac{\sqrt{2}}{2} \cdot \frac{2a}{EA_n} \rightarrow$

$u_x^{(n)}(2) = -0,00283 R$

$u_z^{(n)}(2) = w_R + w_q = -R \frac{\sqrt{2}}{2} \cdot \frac{(2a)^3}{3EI_n} + w_q$



$M_0 = \frac{3qa^2}{2}$

$V_0 = 2a$

$M_y = V_0 x - M_0 - \frac{q}{2} \langle x-a \rangle^2 = 2ax - \frac{3qa^2}{2} - \frac{q}{2} \langle x-a \rangle^2$

$EI_y w'' = -M_y = -\frac{q}{2} (2ax - 3a^2 - \langle x-a \rangle^2)$

$EI_y w' = -\frac{q}{2} (ax^2 - 3a^2x - \frac{1}{3} \langle x-a \rangle^3) + C_1$

$EI_y w = -\frac{q}{2} (a \frac{x^3}{3} - \frac{3}{2} a^2 x^2 - \frac{1}{12} \langle x-a \rangle^4) + C_1 x + C_2$

$x=0 \dots w=0, w'=0 \rightarrow C_1 = C_2 = 0$

$x=2a \dots w = -\frac{q}{2} (a \cdot \frac{8a^3}{3} - \frac{3}{2} a^2 \cdot 4a^2 - \frac{1}{12} a^4)$

$w_q = q \frac{41a^4}{24EI_n}$

$u_z^{(n)}(2) = q \frac{41a^4}{24EI_n} - R \frac{4\sqrt{2}a^3}{3EI_n}$

$u_z^{(n)}(2) = 10,93333 q - 3,01699 R$

fc. 2: $u_{\xi}^p = u_x^{(n)} e_{\xi x} + u_z^{(n)} e_{\xi z}$

$$0,03536 R = \frac{\sqrt{2}}{2} (-0,00283 R + 10,93333 \text{ g} - 3,01699 R)$$

$$R = 3,562 \text{ g}$$