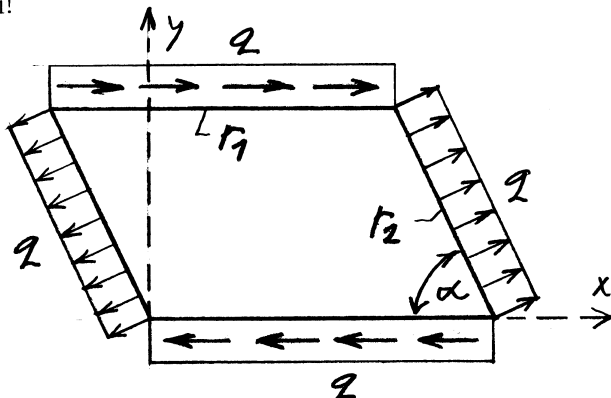


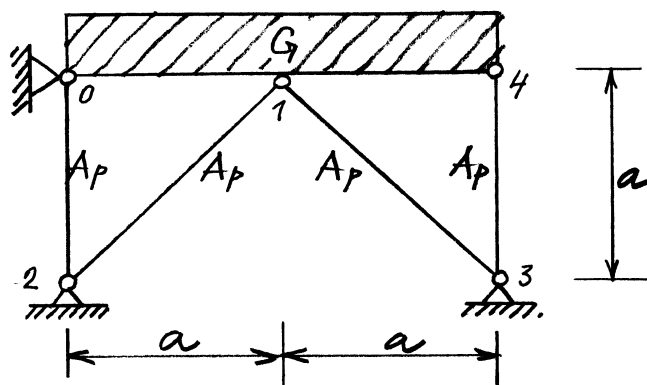
1. Na element enakomerno debele stene deluje zunanja obtežba q , kot kaže skica. Ob predpostavki, da vlada v elementu homogeno ravninsko napetostno stanje, določi kot α , pri katerem je element v ravnotežju! Določi velikosti in smeri glavnih normalnih deformacij v tem primeru ter jih označi na skici!



$E = 200\,000\text{ MPa}$
 $\nu = 0.25$

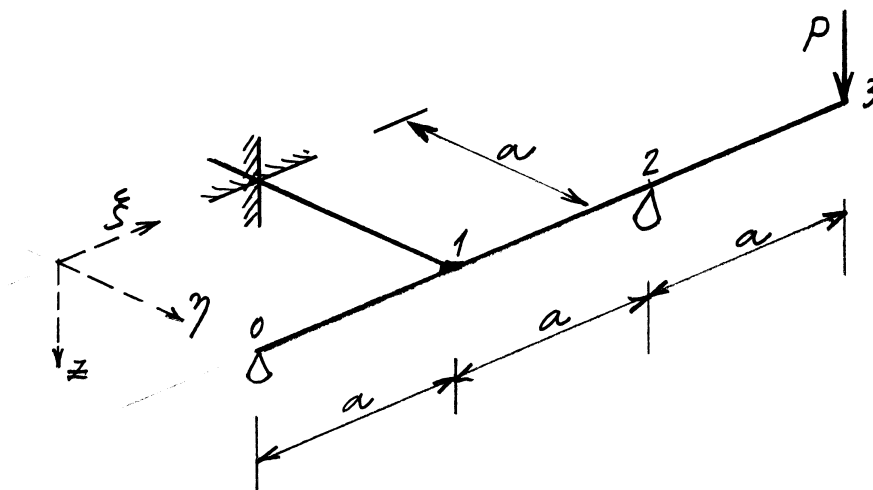
NASVET: Zapiši ravnotežna pogoja na robovih r_1 in r_2 , določi α , nato pa še preostale napetosti!

2. Absolutno toga greda teže G je podprta, kot kaže skica. Določi osne sile v podpornih palicah! Za koliko moramo spremeniti temperaturo palice $\bar{34}$, da v palicah $\bar{12}$ in $\bar{13}$ ne bo napetosti?

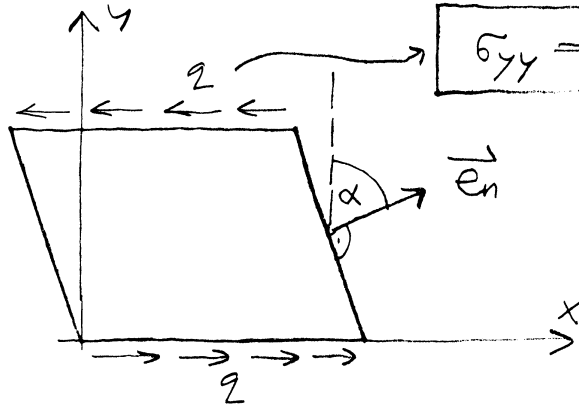


$E = 200\,000\text{ MPa}$
 $\alpha_T = 1.25 \cdot 10^{-5}/\text{K}$
 $a = 2\text{ m}$
 $A_p = 40\text{ cm}^2$
 $G = 0.4\text{ MN}$

3. Določi navpični pomik točke 3! Za vse elemente konstrukcije velja $EI_y = GI_x$. Rezultat izrazi v odvisnosti od obtežbe P !



Ad 1.)



$$\sigma_{yy} = 0, \quad \sigma_{yx} = \sigma_{xy} = \tau$$

$$\begin{aligned} e_{nx} &= \sin \alpha \\ -e_{ny} &= \cos \alpha \\ e_{nz} &= 0 \end{aligned}$$

$$\begin{aligned} \vec{e}_n &= \sin \alpha \vec{e}_x + \cos \alpha \vec{e}_y & \vec{p}_n &= \tau \vec{e}_n \\ \vec{p}_n &= \tau \sin \alpha \vec{e}_x + \tau \cos \alpha \vec{e}_y = \sigma_x e_{nx} + \sigma_y e_{ny} \end{aligned}$$

$$p_{nx} = \tau \sin \alpha = \sigma_{xx} e_{nx} + \sigma_{yx} e_{ny} = \sigma_{xx} \sin \alpha + \tau \cos \alpha$$

$$p_{ny} = \tau \cos \alpha = \sigma_{xy} e_{nx} + \sigma_{yy} e_{ny} = \tau \sin \alpha$$

$$\rightarrow \cos \alpha = \sin \alpha \rightarrow \tan \alpha = 1 \rightarrow \alpha = 45^\circ$$

$$\sin \alpha = \cos \alpha = \frac{\sqrt{2}}{2} \rightarrow \tau \frac{\sqrt{2}}{2} = \sigma_{xx} \frac{\sqrt{2}}{2} + \tau \frac{\sqrt{2}}{2}$$

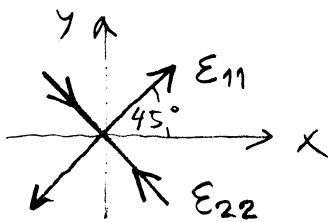
$$\sigma_{xx} = 0$$

$$[\sigma_{ij}] = \begin{bmatrix} 0 & \tau & 0 \\ \tau & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\rightarrow \sigma_{1,2} = \pm \sqrt{\sigma_{xy}^2} = \pm \tau$$

$$\sigma_{11} = \tau, \quad \sigma_{22} = -\tau$$

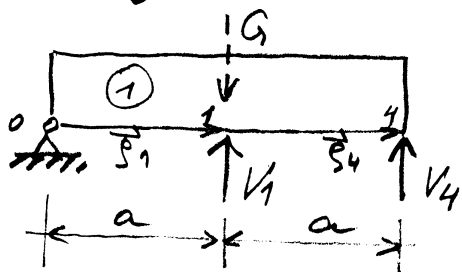
$$\tan 2\alpha_\sigma = \frac{2\sigma_{xy}}{\sigma_{xx} - \sigma_{yy}} = \infty \rightarrow 2\alpha_\sigma = 90^\circ \rightarrow \alpha_\sigma = 45^\circ$$



$$I_1^\sigma = 0$$

$$\begin{aligned} \epsilon_{11} &= \frac{1+\nu}{E} \tau \\ \epsilon_{22} &= -\frac{1+\nu}{E} \tau \\ \epsilon_{33} &= 0 \end{aligned}$$

Ad 2.)



$$\Sigma M^0 = 0 \rightarrow V_1 a + V_4 \cdot 2a - G a = 0$$

$$\boxed{V_1 + 2V_4 = G}$$

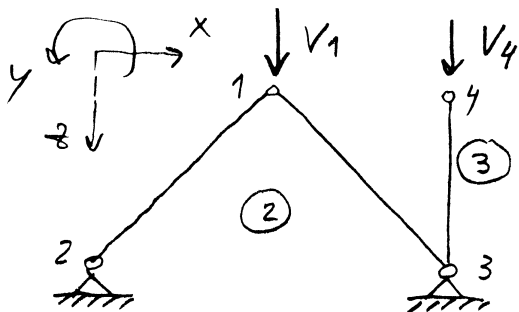
$$\vec{u}_0 = \vec{0}, \quad \vec{\omega}_0 = \omega_y \vec{e}_y$$

$$\vec{p}_1 = a \vec{e}_x, \quad \vec{p}_4 = 2a \vec{e}_x$$

$$\vec{u}_1 = \vec{u}_0 + \vec{\omega}_0 \times \vec{p}_1 = \omega_y \vec{e}_y \times a \vec{e}_x \rightarrow \vec{u}_1 = -a \omega_y \vec{e}_z$$

$w_1^{(1)} = -a \omega_y$	$w_4^{(1)} = -2a \omega_y$
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$$\vec{u}_4 = -2a \omega_y \vec{e}_z$$



$$\boxed{w_4^{(3)} = V_4 \frac{a}{EA \Delta}}$$

$$w_4^{(3)} = \frac{V_4}{4000} = 0,00025 V_4$$

$$\textcircled{2}: l_{12} = l_{13} = a\sqrt{2}$$

$$k_{12} = k_{13} = \frac{EA_p}{a\sqrt{2}} = \frac{20000 \cdot 40}{200\sqrt{2}} = 2828,4 \text{ kN/cm}$$

$$[K_{12}] = 2828,4 \begin{bmatrix} -\frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \\ \frac{\sqrt{2}}{2} & -\frac{\sqrt{2}}{2} \end{bmatrix} \rightarrow [K_{12}] = \begin{bmatrix} 1414,2 & -1414,2 \\ -1414,2 & 1414,2 \end{bmatrix}$$

$$[K_{11}] = \begin{bmatrix} -2828,4 & 0 \\ 0 & -2828,4 \end{bmatrix}$$

$$[K_{13}] = \begin{bmatrix} 1414,2 & 1414,2 \\ 1414,2 & 1414,2 \end{bmatrix}$$

$$[K_{11}] \begin{Bmatrix} u_1 \\ w_1 \end{Bmatrix} + \begin{Bmatrix} 0 \\ V_1 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$

$$\begin{bmatrix} -2828,4 & 0 \\ 0 & -2828,4 \end{bmatrix} \begin{Bmatrix} u_1 \\ w_1 \end{Bmatrix} = \begin{Bmatrix} 0 \\ -V_1 \end{Bmatrix} \rightarrow \begin{cases} u_1^{\textcircled{2}} = 0 \\ w_1^{\textcircled{2}} = \frac{V_1}{2828,4} \end{cases}$$

$$w_1^{\textcircled{1}} = w_1^{\textcircled{2}} \rightarrow -200 w_y = \frac{V_1}{2828,4} = 0,0003536 V_1$$

$$w_4^{\textcircled{1}} = w_4^{\textcircled{3}} \rightarrow -400 w_y = 0,00025 V_4$$

$$w_y = -\frac{V_1}{200} \cdot 0,0003536 = -\frac{V_4}{400} \cdot 0,00025$$

$$1,7678 V_1 = 0,6250 V_4$$

$$V_1 = 0,3536 V_4 = G - 2V_4 \rightarrow 2,3536 V_4 = G$$

$$V_4 = 0,4249 G \rightarrow V_4 = 0,1700 \text{ MN}$$

$$V_1 = G - 2V_4 \rightarrow V_1 = 0,1502 G \rightarrow V_1 = 0,0600 \text{ MN}$$



$$N_{12} = N_{13} = -\frac{V_1}{\sqrt{2}} = \underline{\underline{-0,0424 \text{ MN}}}$$

$$\boxed{\Delta l_{34} = 0} :$$

$$\Delta l_{34} = -\tilde{V}_4 \frac{a}{EA_P} + \alpha_T \Delta T a$$

$$\tilde{V}_4 = \frac{G}{2} \rightarrow$$

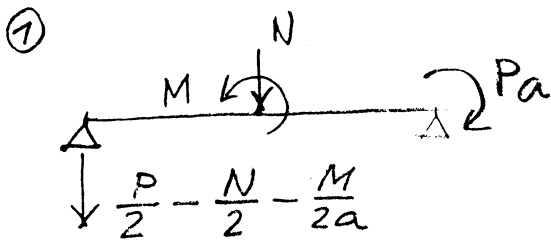
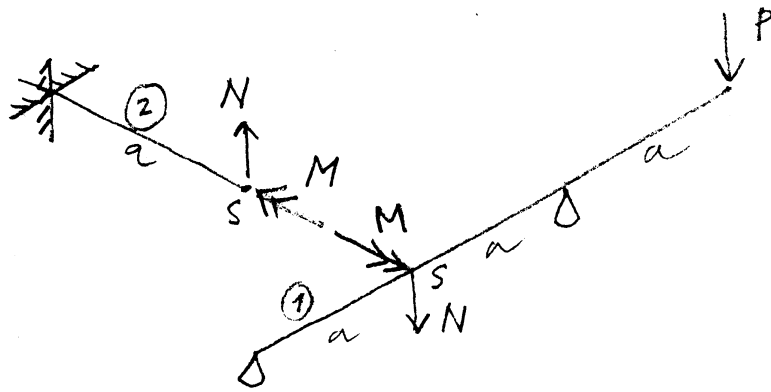
$$G \frac{a}{2EA_P} = \alpha_T \Delta T a$$

$$\boxed{\Delta T = \frac{G}{2EA_P \alpha_T}}$$

$$\rightarrow \Delta T = \frac{400 \cdot 10^5}{2 \cdot 20000 \cdot 40 \cdot 1,25}$$

$$\boxed{\Delta T = 20 \text{ K}}$$

Ad 3)



$$M_y = -\left(\frac{P}{2} - \frac{N}{2} - \frac{M}{2a}\right)x - N\langle x-a \rangle - M\langle x-a \rangle^0 = -EI_y w''''$$

$$EI_y w'''' = \frac{P}{2}x - \frac{N}{2}(x - 2\langle x-a \rangle) - \frac{M}{2a}(x - 2a\langle x-a \rangle)$$

$$EI_y w' = P\frac{x^2}{4} - \frac{N}{2}\left(\frac{x^2}{2} - \langle x-a \rangle^2\right) - \frac{M}{2a}\left(\frac{x^2}{2} - 2a\langle x-a \rangle\right) + C_1$$

$$E I y'''' w = P \frac{x^3}{12} - \frac{N}{2} \left(\frac{x^3}{6} - \frac{1}{3} \langle x-a \rangle^3 \right) - \\ - \frac{M}{2a} \left(\frac{x^3}{6} - a \langle x-a \rangle^2 \right) + C_1 x + C_2$$

$$x=0 \dots N=0 \rightarrow C_2 = 0$$

$$x=2a \dots w=0$$

$$P \cdot \frac{8a^3}{12} - \frac{N}{2} \left(\frac{8a^3}{6} - \frac{a^3}{3} \right) - \\ - \frac{M}{2a} \left(\frac{8a^3}{6} - a^3 \right) + 2a C_1 = 0$$

$$C_1 = -\frac{Pa^2}{3} + \frac{Na^2}{4} + \frac{Ma}{12}$$

$$w_s^{(1)} = -\frac{Pa^3}{4EIy} + \frac{Na^3}{6EIy}$$

$$w_s^{(1)} = \frac{Pa^2}{12EIy} + \frac{Ma}{6EIy}$$

$$(2) \quad w_s^{(2)} = -\frac{Na^3}{3EIy}$$

$$w_s^{(2)} = -\frac{Ma}{GIx}$$

$$w_s^{(1)} = w_s^{(2)} \dots \frac{a^3}{EIy} \left(-\frac{P}{4} + \frac{N}{6} \right) = -\frac{Na^3}{3EIy}$$

$$N = \frac{P}{2}$$

$$w_s^{(1)} = w_s^{(2)} \dots \frac{a}{EIy} \left(\frac{Pa}{12} + \frac{M}{6} \right) = -\frac{Ma}{EIy}$$

$$M = -\frac{Pa}{14}$$

$$V_0 = \frac{P}{2} - \frac{P}{4} + \frac{P}{28} \rightarrow$$

$$V_0 = \frac{2P}{7}$$

