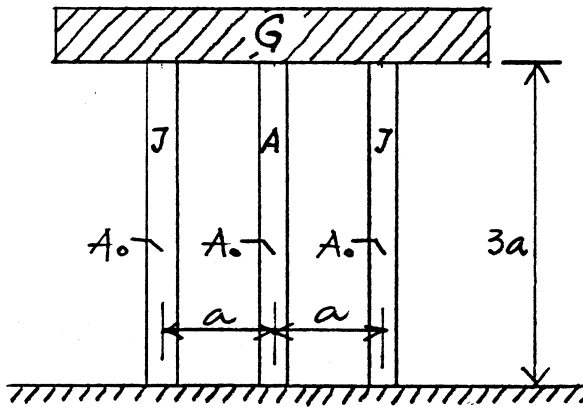


Absolutno togo gredo teže G centrično položimo na tri enako visoke stebre, od katerih je srednji iz aluminija, krajna dva pa sta jeklena. Določi napetosti v stebrih! Za koliko moramo spreminiti temperaturo stebrov, da bodo napetosti v vseh stebrih enake?



$$E_J = 21000 \text{ kN/cm}^2$$

$$E_A = 7000 \text{ kN/cm}^2$$

$$\alpha_J = 1,25 \cdot 10^{-5} / \text{K}$$

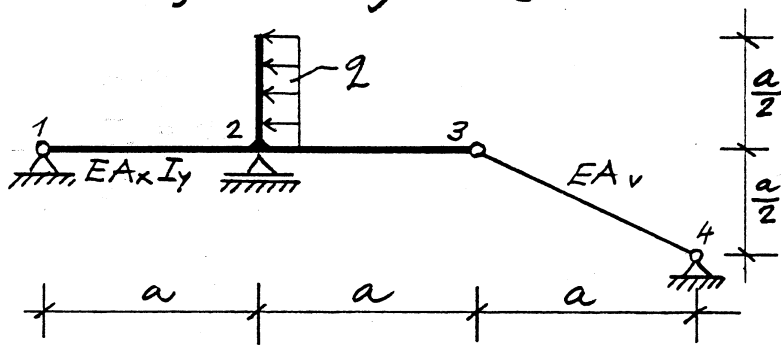
$$\alpha_A = 2 \cdot 10^{-5} / \text{K}$$

$$A_0 = 25,4 \text{ cm}^2$$

$$a = 1 \text{ m}$$

$$G = 300 \text{ kN}$$

2. Dopustni navpični pomik vozlišča 3 je 1 cm. Določi potrebni prečni prerez A_v vrvi 34 ter skiciraj notranje sile!



$$a = 3 \text{ m}$$

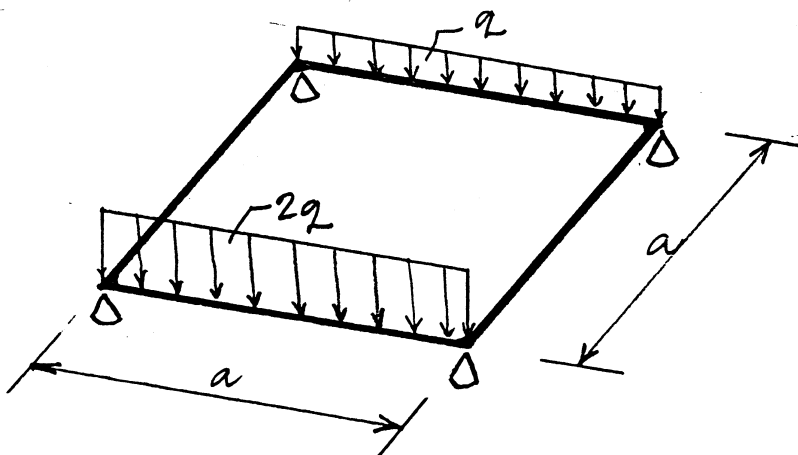
$$A_x = 30 \text{ cm}^2$$

$$I_y = 2000 \text{ cm}^4$$

$$E = 21000 \text{ kN/cm}^2$$

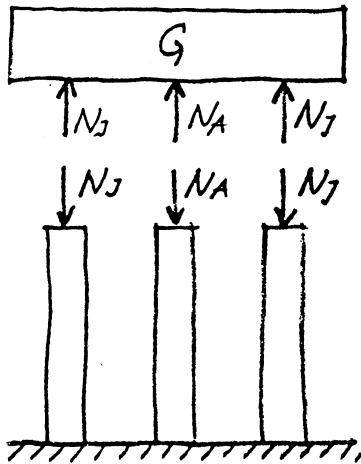
$$q = 120 \text{ kN/m}^1$$

Določi in skiciraj notranje sile!



$$EI_y \approx GI_x$$

Ad 1.)



$$2N_j + N_A = G$$

$$\sigma_j = -\frac{N_j}{A_0} \quad , \quad \sigma_A = -\frac{N_A}{A_0}$$

$$\varepsilon_j = \frac{\sigma_j}{E_j} \quad , \quad \varepsilon_A = \frac{\sigma_A}{E_A}$$

$$\varepsilon_j = \varepsilon_A \rightarrow \sigma_A = \sigma_j \cdot \frac{E_A}{E_j}$$

$$N_j = -A_0 \cdot \sigma_j \quad , \quad N_A = -A_0 \cdot \sigma_j \cdot \frac{E_A}{E_j}$$

$$-2A_0 \cdot \sigma_j - A_0 \cdot \sigma_j \cdot \frac{E_A}{E_j} = G$$

$$\sigma_j = -\frac{G}{A_0} \cdot \frac{E_j}{2E_j + E_A}$$

\$\rightarrow\$

$$\sigma_j = -5,06 \text{ kN/cm}^2$$

$$\sigma_A = -1,69 \text{ kN/cm}^2$$

$$\sigma_A = \sigma_j \rightarrow N_A = N_j = \frac{G}{3} \rightarrow \sigma_A = \sigma_j = -\frac{G}{3A_0}$$

$$\sigma = \sigma_A = \sigma_j = -3,94 \text{ kN/cm}^2$$

$$\varepsilon_j = \frac{\sigma_j}{E_j} + \alpha_j \Delta T \quad , \quad \varepsilon_A = \frac{\sigma_A}{E_A} + \alpha_A \Delta T$$

$$\varepsilon_j = \varepsilon_A \rightarrow \frac{\sigma}{E_j} + \alpha_j \Delta T = \frac{\sigma}{E_A} + \alpha_A \Delta T$$

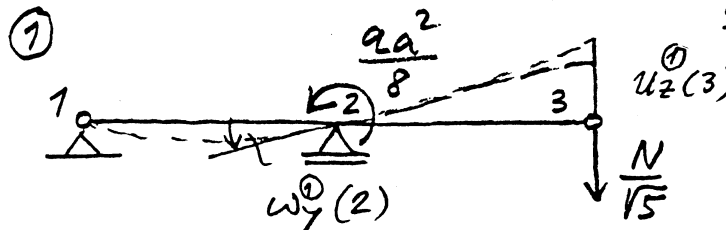
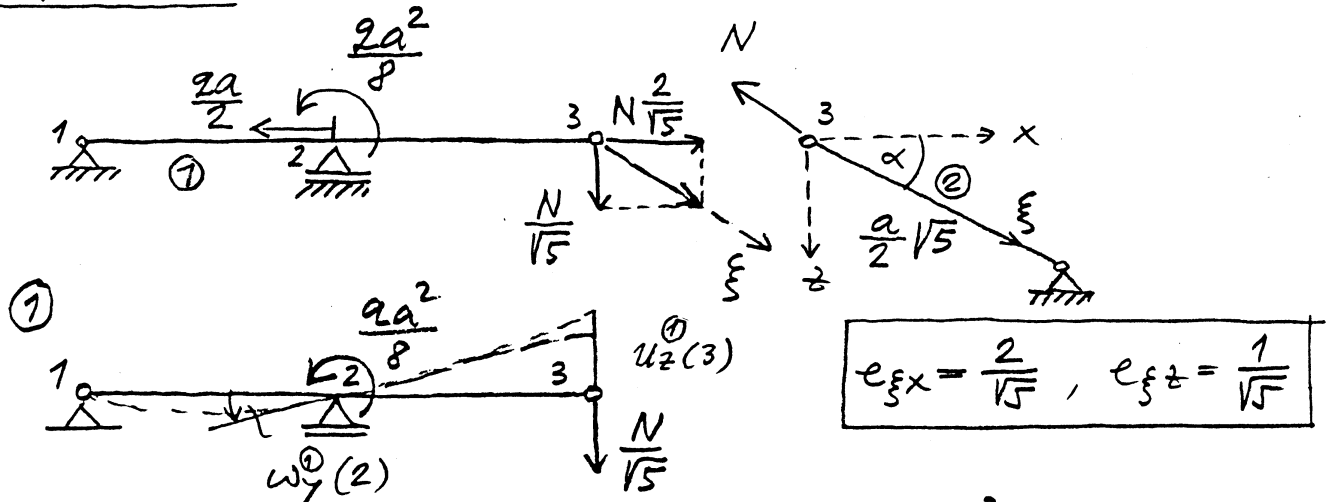
$$\Delta T (\alpha_A - \alpha_j) = \sigma \left(\frac{1}{E_j} - \frac{1}{E_A} \right)$$

$$\Delta T = -\sigma \frac{E_j - E_A}{E_j E_A (\alpha_A - \alpha_j)}$$

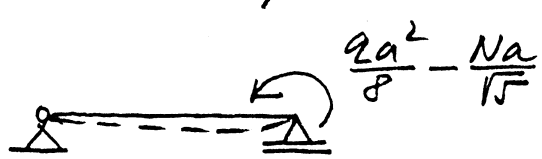
\$\rightarrow\$

$$\Delta T = 50 \text{ K}$$

Ad 2.)



$$e_{\xi x} = \frac{2}{\sqrt{5}}, \quad e_{\xi z} = \frac{1}{\sqrt{5}}$$



$$\omega_y^{(1)}(2) = \left(\frac{2a^2}{8} - \frac{Na}{\sqrt{5}} \right) \cdot \frac{a}{3EI_y}$$

$$u_z^{(1)}(3) = -\omega_y^{(1)}(2) \cdot a + \frac{N}{\sqrt{5}} \cdot \frac{a^3}{3EI_y}$$

$$u_z^{(1)}(3) = -\frac{2a^4}{24EI_y} + \frac{2Na^3}{3\sqrt{5}EI_y}$$

$$u_z^{(1)}(3) = -9,64286 + 0,19166 N$$

$$u_z^{(1)}(3) = -1 \text{ cm} \rightarrow N = 45,095 \text{ kN}$$

$$u_x^{(1)}(3) = \frac{2N}{\sqrt{5}} \cdot \frac{2a}{EA_x} - \frac{2a}{2} \cdot \frac{a}{EA_x}$$

$$u_x^{(1)}(3) = 0,03841 - 0,08571 = -0,04730$$

$$u_{\xi}^{(2)}(3) = -\frac{Na\sqrt{5}}{2EA_V}$$

$$u_{\xi}^{(2)}(3) = -\frac{0,72024}{A_V}$$

V točki 3:

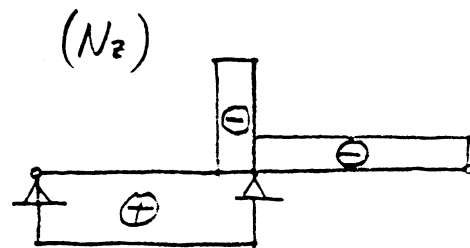
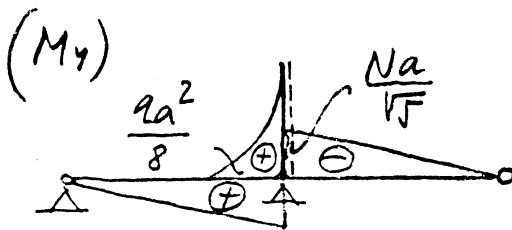
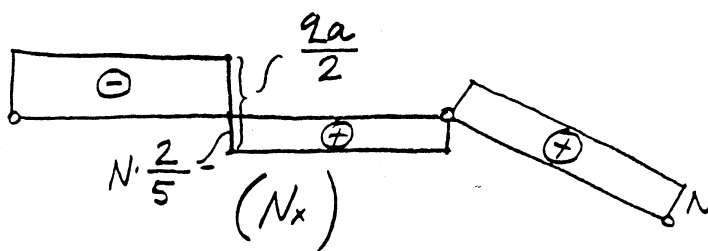
$$u_x^{(1)} e_{\xi x} + u_z^{(1)} e_{\xi z} = u_{\xi}^{(2)}$$

$$-0,04730 \cdot \frac{2}{\sqrt{5}} + (-9,64286 + 0,19166 \cdot 45,095) \cdot \frac{1}{\sqrt{5}} =$$

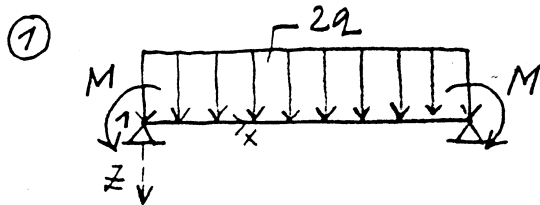
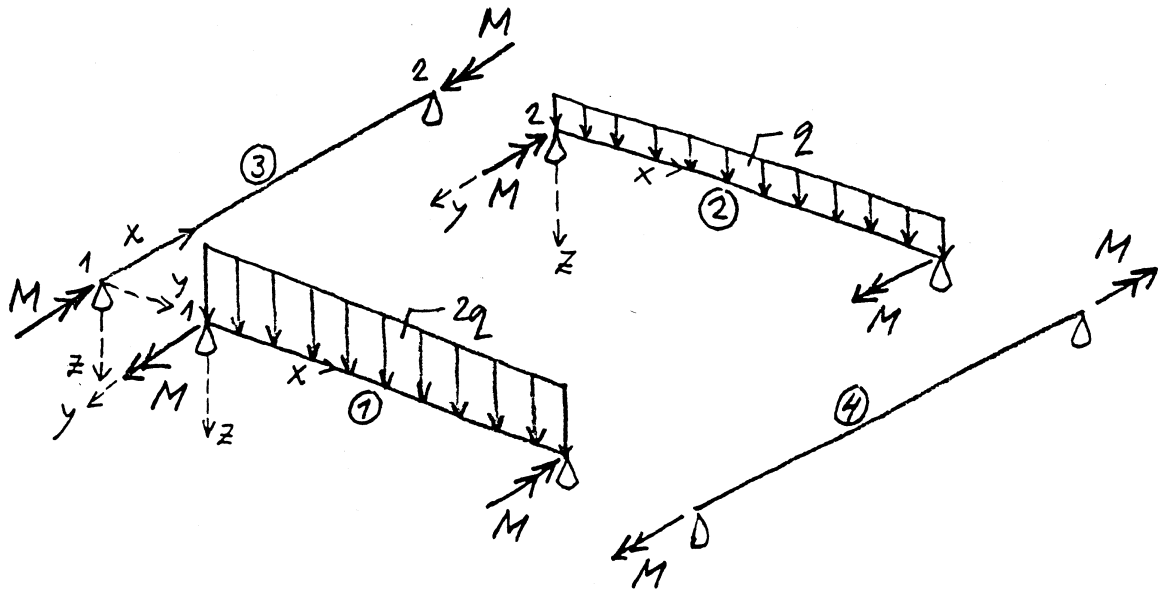
$$= -\frac{0,72024}{A_v}$$

$$-0,04231 - 4,31242 + 3,86520 = -\frac{0,72024}{A_v}$$

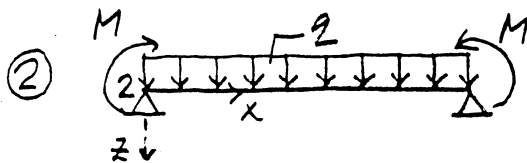
$$A_v = 1,47 \text{ cm}^2$$



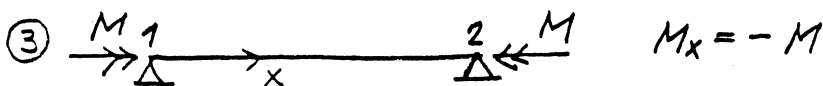
Ad 3.)



$$\omega_y^{(1)} = \frac{Ma}{2EI_y} - \frac{2qa^3}{24EI_y}$$



$$\omega_y^{(2)} = -\frac{Ma}{2EI_y} - \frac{qa^3}{24EI_y}$$



$$\frac{d\omega_x}{dx} = \frac{M_x}{GI_x} = -\frac{M}{GI_x} \rightarrow \omega_x^{(3)} = -\frac{Mx}{GI_x} + C_1$$

$$x=0 \dots \omega_x^{(3)}(1) = -\omega_y^{(1)} \rightarrow C_1 = -\omega_y^{(1)}$$

$$x=a \dots \omega_x^{(3)}(2) = -\omega_y^{(1)} - \frac{Ma}{GI_x} = -\omega_y^{(2)}$$

$$\frac{Ma}{2EI_y} - \frac{2qa^3}{24EI_y} + \frac{Ma}{GI_x} = -\frac{Ma}{2EI_y} - \frac{qa^3}{24EI_y}$$

$$M = \frac{2a^2}{48}$$

