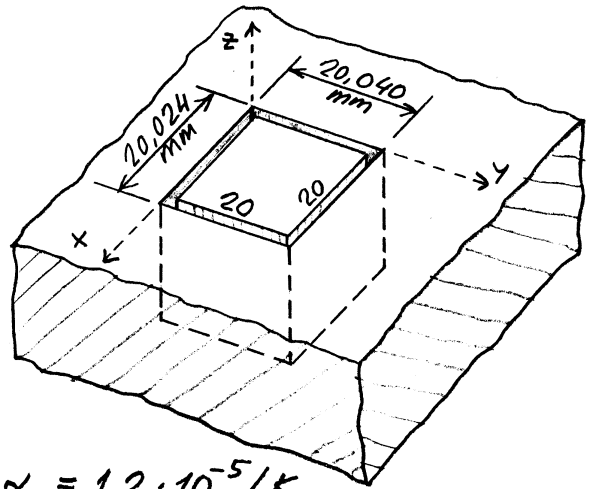


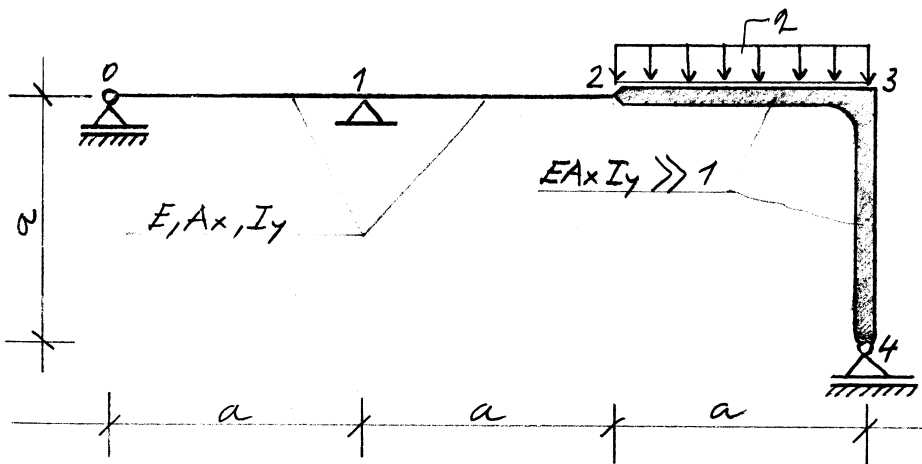
1. Jekleno kocko s stranico dolžine 20 mm centrično vstavimo v absolutno nepodajni utor dimenzij 20,024 x 20,040 x 20 in jo začnemo segrevati. Določi:

- Spremembo temperature, pri kateri se kocka prvič dotakne stene utora.
- Spremembo temperature, pri kateri kocka v celoti zapolni utor.
- Napetosti v kocki, če jo segrejemo za 160 K.



$$E = 20\,000 \text{ kN/cm}^2, \quad \nu = 0.3, \quad \alpha_T = 1.2 \cdot 10^{-5} / \text{K}$$

2. Določi in skiciraj notranje sile!



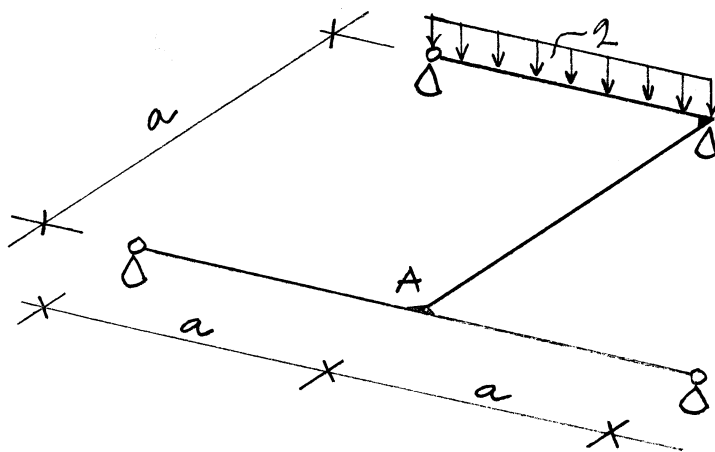
$$E = 20\,000 \text{ kN/cm}^2$$

$$I_y = 6000 \text{ cm}^4$$

$$A_x = 160 \text{ cm}^2$$

$$q = 40 \text{ kN/m}^1$$

3. Določi povos točke A ter skiciraj notranje sile!



$$EI_y = GI_x$$

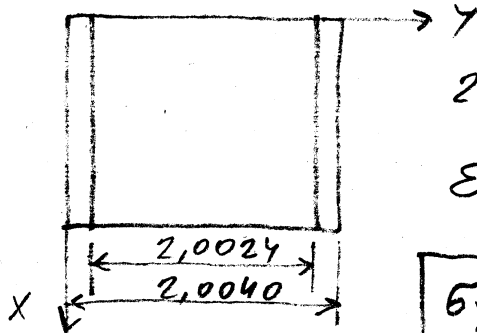
Ad 1Fnote: kN, cm, K

$$a) \quad 2 \cdot (1 + \epsilon_{xx}^a) = 2,0024$$

$$\epsilon_{xx}^a = \frac{2,0024 - 2}{2} = 0,0012$$

$$\epsilon_{xx}^a = \alpha_T \Delta T_a \rightarrow \Delta T_a = \frac{\epsilon_{xx}^a}{\alpha_T} \rightarrow \boxed{\Delta T_a = 100 \text{ K}}$$

b)



$$2,0024 \times (1 + \epsilon_{yy}^b) = 2,0040$$

$$\epsilon_{yy}^b = \frac{2,0040 - 2,0024}{2,0024} = 0,0008$$

$$\boxed{\sigma_{yy} = \sigma_{zz} = 0, \quad \epsilon_{xx} = 0}$$

$$\epsilon_{xx}^b = \frac{1}{E} [\sigma_{xx} - \nu (\sigma_{yy} + \sigma_{zz})] + \alpha_T \Delta T_b^* = 0$$

$$\epsilon_{yy}^b = \frac{1}{E} [\sigma_{yy} - \nu (\sigma_{xx} + \sigma_{zz})] + \alpha_T \Delta T_b^* = 0,0008$$

$$-\frac{\nu \sigma_{xx}}{E} + \alpha_T \Delta T_b^* = \epsilon_{yy}^b$$

$$\frac{\sigma_{xx}}{E} + \alpha_T \Delta T_b^* = 0 \rightarrow \alpha_T \Delta T_b^* = -\frac{\sigma_{xx}}{E}$$

$$-(1 + \nu) \frac{\sigma_{xx}}{E} = \epsilon_{yy}^b \rightarrow \sigma_{xx} = -\frac{20000 \cdot 0,0008}{1,3}$$

$$\boxed{\sigma_{xx}^b = -12,3 \text{ kN/cm}^2}$$

$$\Delta T_b^* = -\frac{\sigma_{xx}}{E \alpha_T} = \frac{12,3}{20000 \cdot 1,2 \cdot 10^{-5}}$$

$$\Delta T_b^* = 51,2 \text{ K}$$

$$\Delta T_b = \Delta T_a + \Delta T_b^* \rightarrow \boxed{\Delta T_b = 151,2 \text{ K}}$$

(2)

$$c) \quad \boxed{\sigma_{zz} = 0} \quad \boxed{\epsilon_{xx} = \epsilon_{yy} = 0} \quad \boxed{\Delta T_c^* = 8,8 \text{ K}}$$

$$\epsilon_{xx}^c = \frac{1}{E} (\sigma_{xx}^c - \nu \sigma_{yy}^c) + \alpha_T \Delta T_c^* = 0$$

$$\epsilon_{yy}^c = \frac{1}{E} (\sigma_{yy}^c - \nu \sigma_{xx}^c) + \alpha_T \Delta T_c^* = 0$$

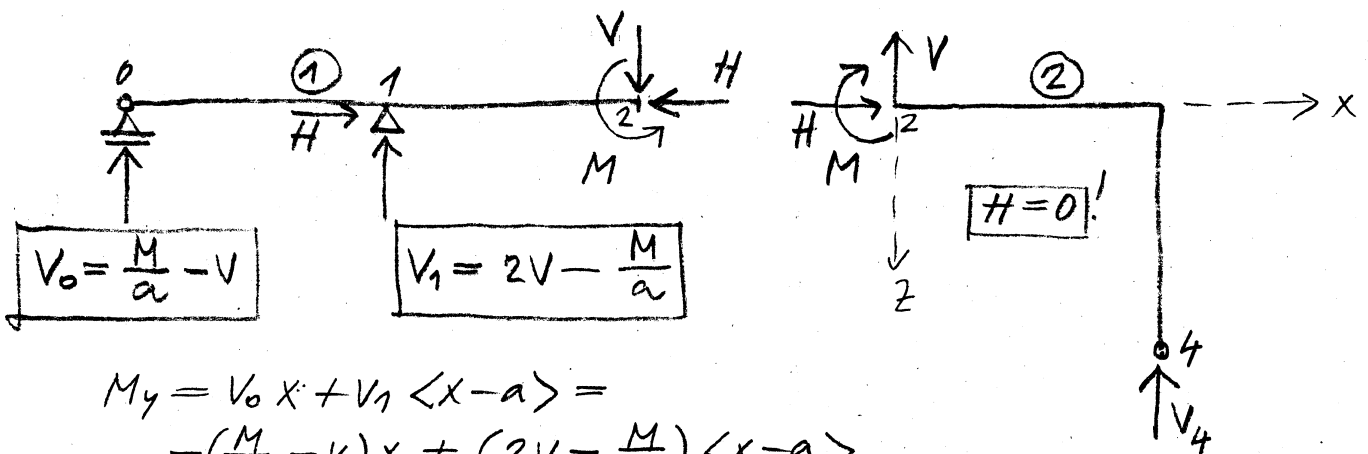
$$\boxed{\sigma_{xx}^c = \sigma_{yy}^c = - \frac{E \alpha_T \Delta T_c^*}{1 - \nu}}$$

$$\sigma_{xx}^c = \sigma_{yy}^c = - \frac{20000 \cdot 1,2 \cdot 10^{-5} \cdot 8,8}{0,7} = 3 \text{ kN/cm}^2$$

$$\boxed{\sigma_{xx}^c = \sigma_{yy}^c = -3,4 \text{ kN/cm}^2}$$

$$\sigma_{xx} = -12,3 - 3,4 \rightarrow \boxed{\begin{aligned} \sigma_{xx} &= -15,3 \text{ kN/cm}^2 \\ \sigma_{yy} &= -3,0 \text{ kN/cm}^2 \\ \sigma_{zz} &= 0 \end{aligned}}$$

Ad 2.)



$$M_y = V_0 x + V_1 \langle x - a \rangle =$$

$$= \left( \frac{M}{a} - V \right) x + \left( 2V - \frac{M}{a} \right) \langle x - a \rangle$$

$$M_y = V(2 \langle x - a \rangle - x) + \frac{M}{a} (x - \langle x - a \rangle) = -EI_y w''$$

$$EI_y w'' = V(x - 2 \langle x - a \rangle) + \frac{M}{a} (\langle x - a \rangle - x)$$

③

$$EI_y w' = V \left( \frac{x^2}{2} - (x-a)^2 \right) + \frac{M}{2a} \left( (x-a)^2 - x^2 \right) + C_1$$

$$EI_y w = V \left( \frac{x^3}{6} - \frac{1}{3} (x-a)^3 \right) + \frac{M}{6a} \left( (x-a)^3 - x^3 \right) + C_1 x + C_2$$

$$x=0 \rightarrow w=0 \rightarrow C_2=0$$

$$x=a \rightarrow w=0 \rightarrow \frac{Va^3}{6} - \frac{Ma^2}{6} + C_1 a = 0$$

$$\boxed{C_1 = \frac{Ma}{6} - \frac{Va^2}{6}}$$

$$x=2a :$$

$$EI_y w_2 = Va^3 \left( \frac{8}{6} - \frac{1}{3} - \frac{1}{3} \right) + \frac{Ma^2}{6} (1 - 8 + 2)$$

$$\boxed{w_2^{(1)} = \frac{2Va^3}{3EI_y} - \frac{5Ma^2}{6EI_y}}$$

$$-EI_y w_2 = Va^2 \left( \frac{4}{2} - 1 - \frac{1}{6} \right) + \frac{Ma}{2} \left( 1 - 4 + \frac{1}{3} \right)$$

$$\boxed{w_2^{(1)} = -\frac{5Va^2}{6EI_y} + \frac{4Ma}{3EI_y}}$$

$$\boxed{u_2^{(1)} = 0}$$

$$\textcircled{2} \quad \Sigma M^4 = 0 \rightarrow M + Va - \frac{2a^2}{2} = 0$$

$$\boxed{M = \frac{2a^2}{2} - Va}$$

$$\boxed{\vec{u}_4^{(2)} = u_4^{(2)} \vec{e}_x \quad \vec{w}_4^{(2)} = w_4^{(2)} \vec{e}_y \quad \vec{r}_2 = -a \vec{e}_x - a \vec{e}_z}$$

$$\vec{u}_2 = u_4^{(2)} \vec{e}_x + w_4^{(2)} \vec{e}_y \times (-a \vec{e}_x - a \vec{e}_z)$$

$$\vec{u}_2 = u_4^{(2)} \vec{e}_x + a w_4^{(2)} \vec{e}_z - a w_4^{(2)} \vec{e}_y$$

$$\boxed{\vec{u}_2 = (u_4^{(2)} - a w_4^{(2)}) \vec{e}_x + a w_4^{(2)} \vec{e}_z}$$

$$\boxed{\vec{w}_2 = w_4^{(2)} \vec{e}_y}$$

$$w_4^{(2)} = w_2^{(1)} = -\frac{5Va^2}{6EI_y} + \frac{4a}{3EI_y} \left( \frac{2a^2}{2} - Va \right)$$

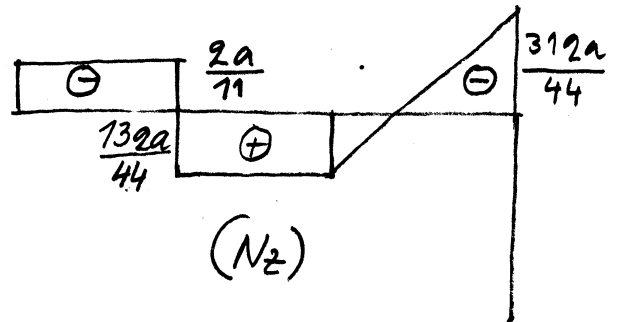
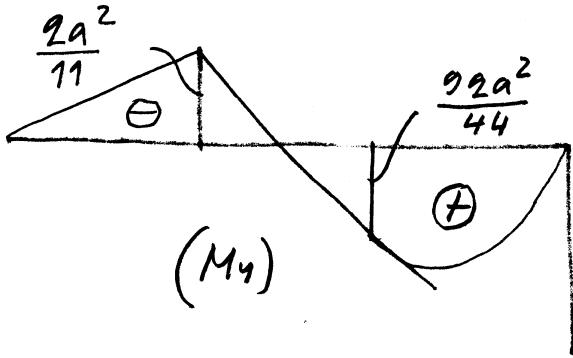
$$\boxed{w_4^{(2)} = -\frac{13Va^2}{6EI_y} + \frac{2a^3}{3EI_y}}$$

$$w_2^{(1)} = \frac{2Va^3}{3EI_y} - \frac{5a^2}{6EI_y} \left( \frac{2a^2}{2} - Va \right) = a \left( \frac{13Va^2}{6EI_y} + \frac{22a^3}{3EI_y} \right) \quad (4)$$

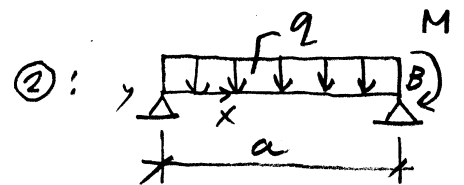
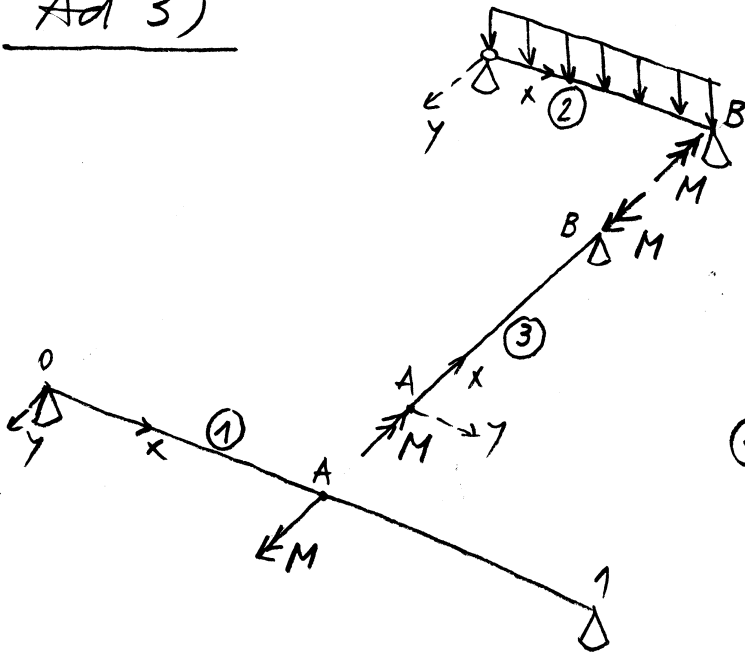
$$\frac{11Va^3}{3} = \frac{132a^4}{12} \rightarrow V = \frac{132a}{44}$$

$$M = \frac{2a^2}{2} - \frac{13}{44} 2a^2 \rightarrow M = \frac{92a^2}{44}$$

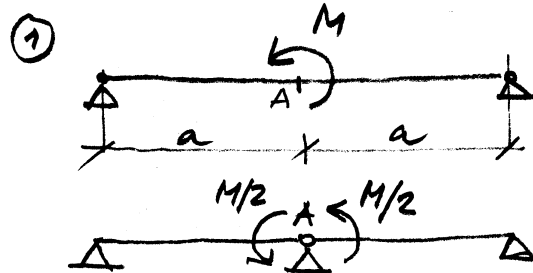
|                        |                         |                         |
|------------------------|-------------------------|-------------------------|
| $V_0 = -\frac{2a}{11}$ | $V_1 = \frac{172a}{44}$ | $V_4 = \frac{312a}{44}$ |
|------------------------|-------------------------|-------------------------|



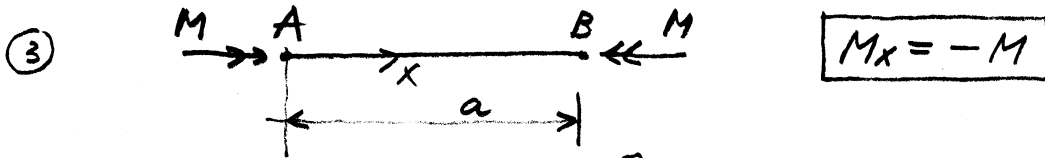
Ad 3)



$$w_y^{(2)}(B) = \frac{2a^3}{24EI_y} - \frac{Ma}{3EI_y}$$



$$w_y^{(1)}(A) = \frac{Ma}{6EI_y}$$



$$\omega_x^{(3)}(B) = \omega_x^{(3)}(A) + a\alpha = \omega_x^{(3)}(A) - \frac{Ma}{GI_x}$$

$$\omega_x^{(3)}(A) = -\omega_y^{(2)}(A)$$

$$\omega_x^{(3)}(B) = -\omega_y^{(2)}(B)$$

$$-\frac{2a^3}{24EI_y} + \frac{Ma}{3EI_y} = -\frac{Ma}{6EI_y} - \frac{Ma}{GI_x}$$

$$EI_y = GI_x \rightarrow M = \frac{2a^2}{36}$$

